

Performance of Wall Confluent Jets Ventilation System in School Environment compared with Displacement Ventilation

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School ventilation: challenging from thermal comfort and air quality considerations

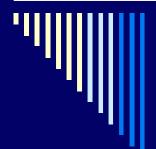
- In schools, the number of students per square metre of floor area has increased during the last decade.
- Increase in heat load has caused indoor climate problems in schools.
- □ Ventilation systems that have been designed for other applications may not perform well in school buildings.



Supply Methods

The method of supplying conditioned air to a room or a zone in a building has a direct impact on:

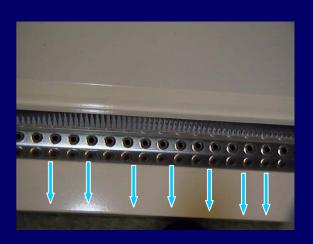
- √ The air quality in the zone
- √The thermal comfort in the zone
- √The energy consumption of the HVAC system
- √The facility management schedules



Definition

- In ventilation, a confluent jet is formed, when circular jets issuing from different apertures in the same plane flow in parallel directions, and at a certain distance downstream they coalesce and move as a single jet.
- Two type of configurations:
 - (a) Ceiling level
 - (b) floor level (blowing to the wall)





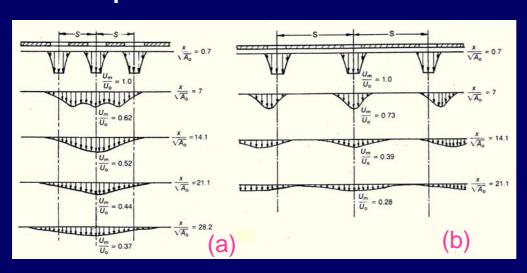
(b)

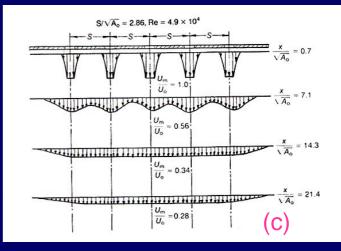




Spacing: Confluent Jets

☐ The distance from the outlets at which the jets merge depends on the distance between and the area of the outlets.





Velocity profiles for confluent circular jets. (a) Closely-spaced

$$S/\sqrt{A_o} = 2.8$$
, Re= 8×10^4

(b) widely-spaced

$$S/\sqrt{A_o} = 5.6$$
, Re= 5.8×10^4

Awbi (2003)

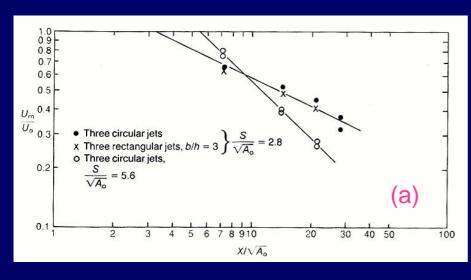
(c) Velocity profiles for five confluent circular jets

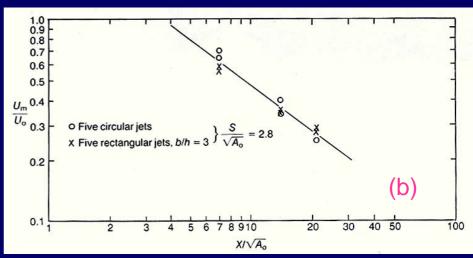
$$S/\sqrt{A_o} = 2.86$$
, Re= 4.9×10^4



Definition: Confluent Jets /Con...

Awbi (2003)





- (a) Velocity decay for three confluent jets (circular & rectangular openings).
- (b) Velocity decay for five confluent jets (circular & rectangular openings).



MECHANICAL VENTILATION

Mixing Air Distribution

A mixing ventilation system aims to dilute the indoor pollutants by mixing fresh air with room air. Usually, an air jet is supplied at high level to achieve the mixing and provide acceptable velocities at low level. Ventilation efficiency < 50% (if one choose 50% as perfect mixing!!!).

Displacement Ventilation

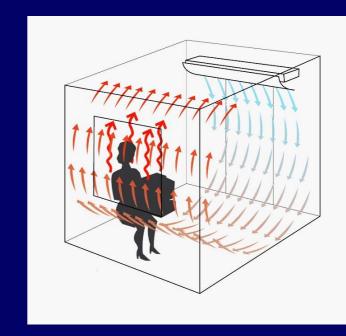
Here, air is usually supplied directly into the occupied zone at low velocity and heat and indoor pollutants are displaced upwards due to the plumes rising above heat sources in the room. The ventilation efficiency is usually >>50%.

Wall DV units are only suitable for small cooling loads (<40W/m²) and for higher loads chilled ceiling panels or chilled beams are used to supplement the cooling.



Confluent Jets Ventilation

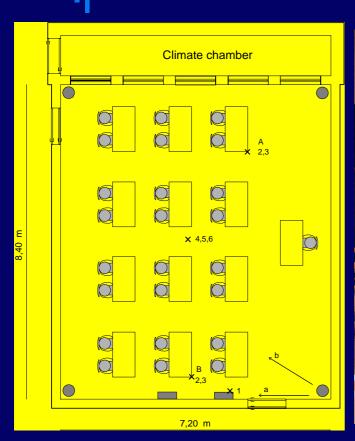
- Here a jet of air is supplied downward on to the floor with quite a high momentum (i.e. resembling mixing ventilation) but the velocity decays very rapidly away from the point of impact on the floor. This method is suitable for cooling and heating.
- The ventilation efficiency is usually >>50%.
- Confluent jets units are suitable for high cooling loads (>40W/m²; 60W/m² was tested in Reading climate chamber).



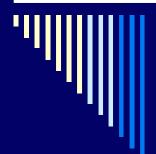


BMG Lab. Gävle, Sweden

a Teacher & 24 Students







Heat Loads

Classroom Loads used in the CFD simulations

(8.4*7.2*3 m)

| Load | Surface Area [m ²] | Cooling Load | Heating Load |
|---|--------------------------------|--------------------|-----------------------|
| Window gain (loss) 25 person simulators Light (9 lamps) | 7.9 1.69 each 0.87 each | 776 2375 525 | (-517) 2375 525 |
| Total (W) | | 3676 | 2383 |
| Total (W/m²) | | 63 | 41 |

B.C.: Inlet velocity and wall temperatures were obtained from measurements



We need parameters to compare systems

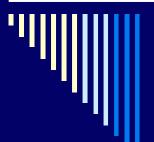
Fangers Definitioner (ISO 7730; 1994)

Percentage of dissatisfied with the indoor air quality:

$$PD = 395 \cdot \exp\left(-1.83\dot{v}^{0.25}\right)$$

Percentage of dissatisfied with the thermal environment:

$$PPD = 100 - \exp{-\left\{0.03353(PMV)^4 + 0.2179(PMV)^2\right\}}$$



Definitions & ADI (Air Quality Index), Ventilation Parameter

Ventilations Efficiency for Heat Removal:

$$\varepsilon_{t} = \frac{T_{o} - T_{i}}{\overline{T} - T_{i}}$$

Ventilations Effectiveness for Contaminant Removal:

$$\varepsilon_c = \frac{C_o - C_i}{\overline{C} - C_i}$$

Thermal comfort Number:

$$N_{t} = \frac{\mathcal{E}_{t}}{PPD}$$

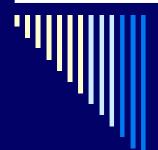
Air Quality Number:

$$N_c = \frac{\mathcal{E}_c}{PD}$$



Ventilations Parameter (VP) or Air Distribution Index (ADI)

$$ADI = \sqrt{N_t \times N_c}$$

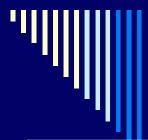


Measurements in Classroom BMG, Gävle

| Case | No. of Terminals x flow rate [l/s] | Position (See FIG.) | Local Air F | exchange Index | Air Exchange Effectiveness $\frac{\tau_n}{2\left\langle \overline{\tau} \right\rangle} \times 100$ | | | | |
|-----------|--|------------------------|-------------|----------------|--|-------------|-----------|------|-----|
| | | | Point no. | Point no. 3 | Point no. 4 | Point no. 5 | Point no. | EXP. | CFD |
| DV4C_A50 | 4 x 50 | A+middle | 1.28 | 0.68 | 1.19 | 0.95 | 0.79 | 43 | 48 |
| CF4C_A50 | 4 x 50 | A+middle | 1.195 | 1.155 | 1.32 | 1.35 | 1.145 | 56 | 54 |
| CF4C_B50 | 4 x 50 | B+middle | 1.48 | 1.28 | 1.10 | 1.19 | 1.06 | 73 | 54 |
| CF4C_B3 | 4 x 32 | B+middle | 1.755 | 1.61 | 1.43 | 1.36 | 1.26 | 50 | 52 |
| CF2_B60 | 2 x 60 | B+middle | 1.75 | 1.52 | 1.58 | 1.43 | 1.22 | 51 | 50 |
| CF2C_B100 | 2 x 100 | B+middle | 1.20 | 1.1 | 1.11 | 1.12 | 1.01 | 51 | 52 |

DV = Displacement system

CF= Confluent Jets System

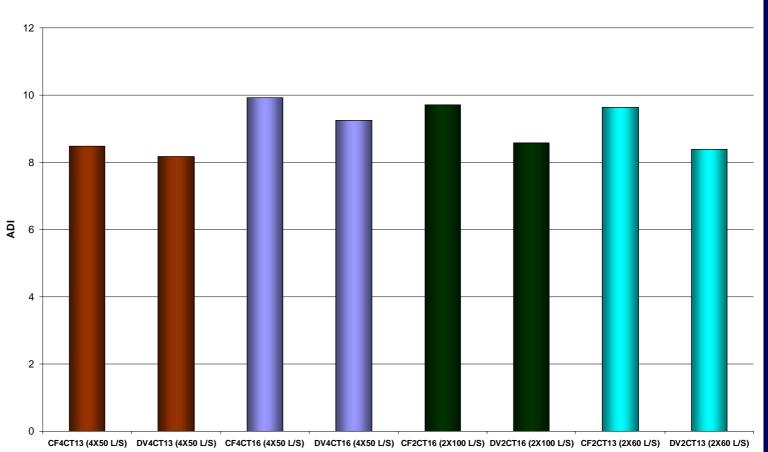


| | | COMFORT AND AIR (| QUALITY | | Vortex version | Case | No of device | |
|-------------------------------------|----------------------------------|--|---|---|----------------|--------------|--------------------------|--|
| VENTILATION EFFECTIVENESS [%] | VENTILATION EFFICIENCY [%] | COMFORT NUMBER FOR AIR QUALITY [-] | COMFORT NUMBER FOR THERMAL SENSATION [-] | AIR DISTRIBUTION INDEX (ADI)) [-] | | | Times flow rate (l/s) | |
| 102.3 | 105.1 | 5.622 | 12.74 | 8.464 | Vortex3Cκ-ε | CF4CT13 | 4 x 50 | |
| 98.46 | 99.50 | 5.411 | 12.37 | 8.180 | Vortex3Cκ-ε | DV4CT13 | 4 x 50 | |
| 107.8 | 125.1 | 5.922 | 16.65 | 9.931 | Vortex3Cκ-ε | CF4CT16 | 4 x 50 | |
| 113.6 | 129.8 | 6.245 | 16.75 | 10.23 | V4D-RNG | CF4CT16 | 4 x 50 | |
| 98.43 | 113.5 | 5.409 | 15.83 | 9.253 | Vortex3Cκ-ε | DV4CT16 | 4 x 50 | |
| 101.6 | 115.0 | 5.583 | 15.69 | 9.359 | V4D-RNG | DV4CT16 | 4 x 50 | |
| 111.8 | 98.06 | 6.144 | 12.19 | 8.654 | Vortex3Cκ-ε | CF2CT13 | 2 x 100 | |
| 94.82 | 91.92 | 5.211 | 11.66 | 7.795 | Vortex3Cκ-ε | DV2CT13 | 2 x 100 | |
| 108.3 | 114.0 | 5.954 | 15.81 | 9.702 | Vortex3Cκ-ε | CF2CT16 | 2 x 100 | |
| 92.07 | 145.2 | 5.060 | 14.53 | 8.574 | Vortex3Cκ-ε | DV2CT16 | 2 x 100 | |
| 119.5 | 121.5 | 6.570 | 16.10 | 10.28 | V4D-RNG | CF2CT16 | 2 x 100 | |
| 113.5 | 163.8 | 4.506 | 19.66 | 9.412 | Vortex3Cκ-ε | CF4T13 30Lit | 4 x 30 | |
| 117.5 | 165.4 | 4.466 | 20.79 | 9.636 | Vortex3Cκ-ε | CF2T13 60Lit | 2 x 60 | |
| 98.83 | 128.8 | 3.756 | 18.69 | 8.379 | Vortex3Cκ-ε | DV2T13 60Lit | 2 x 60 | |

CF = Confluent Jets DV= Displacement T16 - T13 = Supply temp 16°C and 13°C respectively





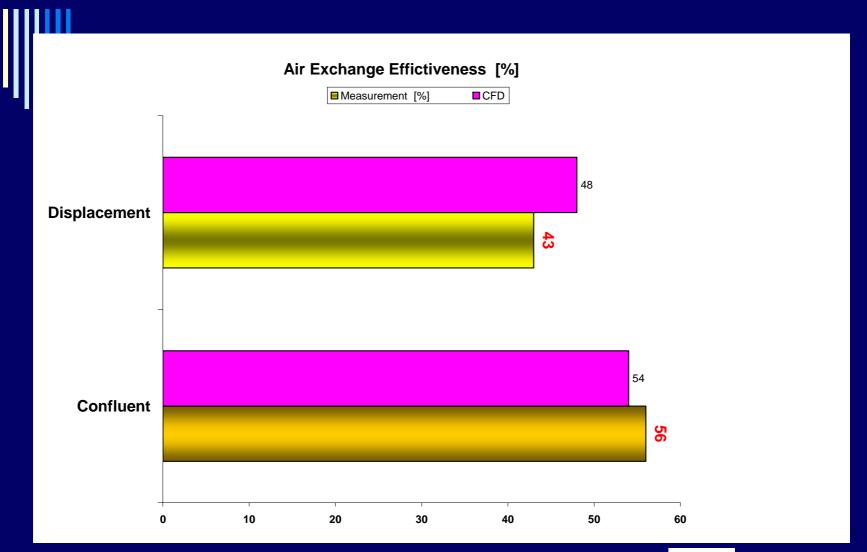




Measured and calculated velocities [m/s] and Temperatures [°C] for Confluent Jets Supply terminal, Case CF4CT16, Four device placed at the corners and

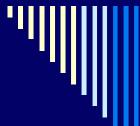
the flow rate of 50 l/s for each device Distance from the wall is 3 cm.

| Height | | Distance from supply (m), along the directions shown by the arrows in Fig. 3 | | | | | | | | | | | |
|-----------------------|------------|--|-----------------------------|--------------|-----------------------------|--------------|-----------------------------|--------------|-----------------------------|--------------|-----------------------------|--------------|-----------------------------|
| above floor (m) | | 0.5 | | 1.0 | | 1.5 | | 2.0 | | 2.5 | | 3.0 | |
| | | Temp (°C) | Vel. (ms ⁻¹) | Temp (°C) | Vel. (ms ⁻¹) | Tem p (°C) | Vel. (ms ⁻¹) | Temp (°C) | Vel. (ms ⁻¹) | Temp (°C) | Vel. (ms ⁻¹) | Temp (°C) | Vel. (ms ⁻¹) |
| 0.10 | Exp. | 19.5 | 0.65 | 19.9 | 0.55 | 20.3 | 0.48 | 20.5 | 0.47 | 20.6 | 0.43 | 21.0 | 0.33 |
| | κ-ε RNG | 19.2 19.0 | 0.6 0.56 | 20.1 19.7 | 0.40 0.57 | 20.2 20.6 | 0.35 0.51 | 21.2 21.1 | 0.32 0.39 | 21.3 21.3 | 0.30 0.32 | 21.7 21.6 | 0.29 0.34 |
| 0.25 | Exp. | 19.7 | 0.59 | 20.2 | 0.59 | 20.5 | 0.46 | 20.6 | 0.41 | 21.0 | 0.32 | 21.2 | 0.24 |
| | κ-ε RNG | 19.8 19.6 | 0.31 0.45 | 21.6 21.4 | 0.36 0.51 | 21.9 21.9 | 0.29 0.42 | 22.1 22.0 | 0.21 0.39 | 22.1 22.0 | 0.20 0.30 | 22.1 22.0 | 0.10 0.20 |
| 0.40 | Exp. | 19.8 | 0.88 | 20.3 | 0.64 | 20.8 | 0.43 | 21.0 | 0.36 | 21.2 | 0.29 | 21.4 | 0.21 |
| | κ-ε RNG | 22.5 22.3 | 0.35 0.70 | 21.9 21.6 | 0.31 0.52 | 22.0 21.7 | 0.25 0.39 | 22.1 21.8 | 0.18 0.30 | 22.2 22.0 | 0.18 0.20 | 22.3 22.1 | 0.08 0.18 |
| 0.60 | Exp. | 20.3 | 0.66 | 20.6 | 0.59 | 21.0 | 0.40 | 21.2 | 0.29 | 21.4 | 0.25 | 21.6 | 0.19 |
| | κ-ε RNG | 22.6 22.6 | 0.30 0.58 | 22.5 22.4 | 0.21 0.55 | 22.4 22.2 | 0.25 0.36 | 22.3 22.3 | 0.10 0.30 | 22.5 22.3 | 0.06 0.20 | 22.5 22.3 | 0.08 0.15 |
| 0.80 | Exp. | 20.6 | 0.54 | 21.0 | 0.52 | 21.3 | 0.32 | 21.5 | 0.26 | 21.7 | 0.22 | 21.9 | 0.15 |
| | κ-ε RNG | 22.7 22.7 | 0.11 0.46 | 22.8 22.6 | 0.15 0.41 | 22.8 22.5 | 0.10 0.28 | 22.8 22.6 | 0.08 0.23 | 22.7 22.5 | 0.03 0.19 | 22.7 22.5 | 0.03 0.09 |

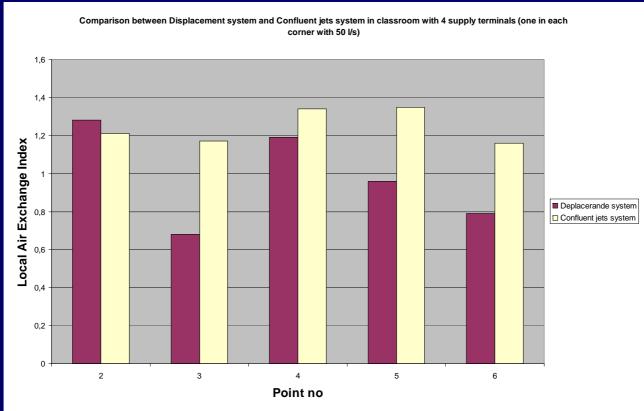


Air exchange effectiveness:

 $\frac{\tau_n}{2\Box\!\left\langle\overline{\tau}\right\rangle}$



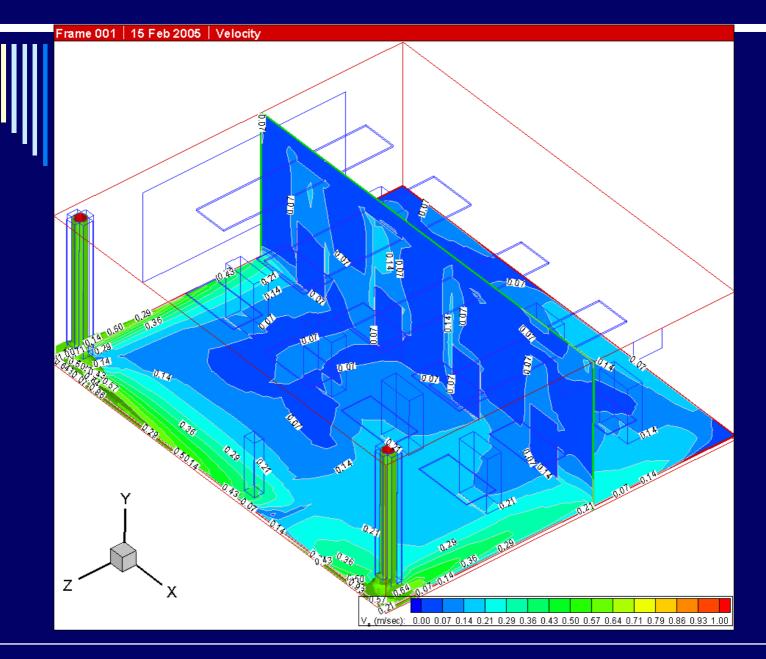
Measurements in BMG classroom, Gävle

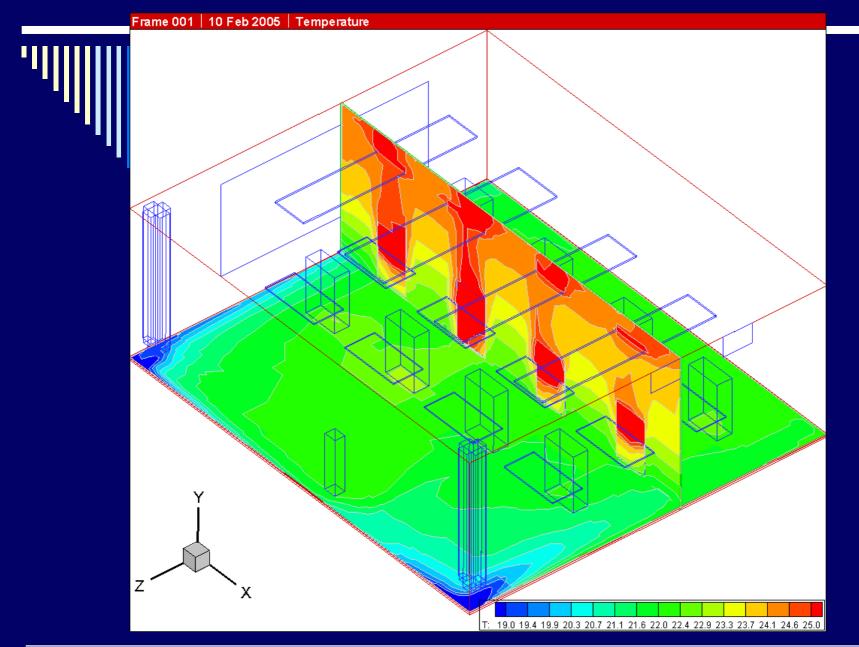


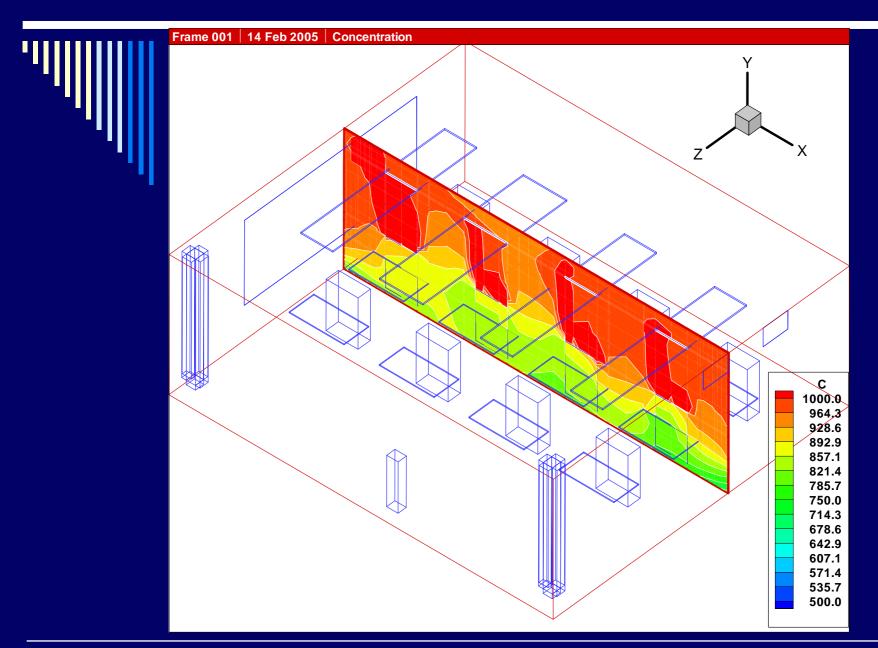
Local Air Exchange >1 Good Air Exchange

 $\frac{\tau_n}{\tau_p}$

Def.: Local Air Exchange Index=(Nominal time constant)/(Local mean age at the point)









Conclusions

- The Wall Confluent Jets Ventilation System is a promising system for use in schools.
- The RNG turbulence model (κ-ε model as well) gives promising results for room air flow pattern.
- One should be careful about the errors in measurements particularly resulting from the short air velocity sampling period.
- Wall confluent jets can successfully be used for both heating and cooling – a combined effect of mixing and displacement systems.
- CFD can be used successfully in predicting thermal comfort and air quality for indoor air climate.